# 3-PRR parallel chain manipulator Project Report MAE 593

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#### Introduction:

The 3PRR parallel chain manipulator has an analytical solution.

 $X_{EE} = D_i \cos \theta_{1i} + L_{1i} \cos \theta_{2i} + L_{2i} \cos \theta_{3i} + X_{Bi} (i = 1, 2, 3)$   $Y_{EE} = D_i \sin \theta_{1i} + L_{1i} \sin \theta_{2i} + L_{2i} \sin \theta_{3i} + Y_{Bi} (i = 1, 2, 3)$  $\phi_{EE} = \theta_{3i} + \delta_{3i} (i = 1, 2, 3)$ 

Thus for given  $(X_{EE}, Y_{EE}, \emptyset_{EE})$  we can solve for  $(D_i, \theta_{2i})$  in case of inverse kinematics and vice versa for forward kinematics.

$$D_i \cos \theta_{1i} + L_{1i} \cos \theta_{2i} = X_{EE} - X_{Bi} - L_{2i} \cos \theta_{3i}$$
$$D_i \sin \theta_{1i} + L_{1i} \sin \theta_{2i} = Y_{EE} - Y_{Bi} - L_{2i} \sin \theta_{3i}$$

Differentiating with respect to time gives

$$\dot{D}_{i} \cos \theta_{1i} - L_{1i} \sin \theta_{2i} \dot{\theta}_{2i} = \dot{X}_{EE} + L_{2i} \sin \theta_{3i} \dot{\theta}_{3i} (i = 1, 2, 3)$$
$$\dot{D}_{i} \sin \theta_{1i} + L_{1i} \cos \theta_{2i} \dot{\theta}_{2i} = \dot{Y}_{EE} - L_{2i} \cos \theta_{3i} \dot{\theta}_{3i} (i = 1, 2, 3)$$
$$\dot{\theta}_{3i} = \dot{\phi}_{EE} (i = 1, 2, 3)$$

Thus we have,

$$\begin{aligned} & \left( \begin{matrix} \dot{D}_{1} \\ \dot{D}_{2} \\ \dot{D}_{3} \\ \dot{\theta}_{21} \\ \dot{\theta}_{22} \\ \dot{\theta}_{23} \end{matrix} \right) + B * \begin{pmatrix} \dot{X}_{EE} \\ \dot{Y}_{EE} \\ \dot{\phi}_{EE} \end{pmatrix} = 0 \\ \\ where \ A = \begin{pmatrix} 1 & 0 & -L_{21} \sin \theta_{31} \\ 1 & 0 & -L_{22} \sin \theta_{32} \\ 1 & 0 & -L_{23} \sin \theta_{33} \\ 0 & 1 & L_{21} \cos \theta_{31} \\ 0 & 1 & L_{22} \cos \theta_{32} \\ 0 & 1 & L_{23} \cos \theta_{33} \end{pmatrix} \end{aligned}$$

$$and \ B = \begin{bmatrix} \cos \theta_{11} & 0 & 0 & -L_{11} \sin \theta_{21} & 0 & 0 \\ 0 & \cos \theta_{12} & 0 & 0 & -L_{12} \sin \theta_{22} & 0 \\ 0 & 0 & \cos \theta_{13} & 0 & 0 & -L_{13} \sin \theta_{23} \\ \sin \theta_{11} & 0 & 0 & L_{11} \cos \theta_{21} & 0 & 0 \\ 0 & \sin \theta_{12} & 0 & 0 & L_{12} \cos \theta_{22} & 0 \\ 0 & 0 & \sin \theta_{13} & 0 & 0 & L_{13} \cos \theta_{23} \end{bmatrix}$$

and J = -inverse(B) \* A

#### Forward Kinematics



 $(D_1, D_2, D_3) = (3.44, 2.93, 2.38), (\theta_{11}, \theta_{12}, \theta_{13})$ = (40.11, 140.83, 270)

#### Inverse Kinematics:



## Workspace:



## Circle Tracing:



## Ellipse Tracing:



#### <u>Control</u>:

## The *Jacobian J and inverse(J*) are given by

J = -inverse(B) \* A

inverse(J) = -inverse(A) \* B

	/1	0	$-L_{21}\sin\theta_{31}$
where A =	1	0	$-L_{22}\sin\theta_{32}$
	1	0	$-L_{23}\sin\theta_{33}$
	0	1	$L_{21}\cos\theta_{31}$
	0	1	$L_{22}\cos\theta_{32}$
	$\setminus 0$	1	$L_{22}\cos\theta_{22}$

and B =

$/\cos\theta_{11}$	0	0	$-L_{11}\sin\theta_{21}$	0	0
0	$\cos \theta_{12}$	0	0	$-L_{12}\sin\theta_{22}$	0
0	0	$\cos \theta_{13}$	0	0	$-L_{13}\sin\theta_{23}$
$\sin \theta_{11}$	0	0	$L_{11}\cos\theta_{21}$	0	0
0	$\sin \theta_{12}$	0	0	$L_{12}\cos\theta_{22}$	0
\ 0	0	$\sin \theta_{13}$	0	0	$L_{13}\cos\theta_{23}$

#### 1) Open Loop Control:

Open loop control was achieved using the *matlab ode*45 function.

$$\dot{\theta}_{openloop} = inverse(J) * \begin{pmatrix} \dot{X}_{EE} \\ \dot{Y}_{EE} \\ \dot{\phi}_{EE} \end{pmatrix}$$

$$\dot{\theta}_{openloop} = -inverse(B) * A * \begin{pmatrix} \dot{X}_{EE} \\ \dot{Y}_{EE} \\ \dot{\phi}_{EE} \end{pmatrix}$$





Please see drop box folder for code for open loop control.



Please see drop box folder for code for open loop control.

2) Closed Loop Control (Joint Space):

$$\begin{split} \dot{\theta}_{openloop} &= -inverse(B) * A * \begin{pmatrix} \dot{X}_{EE} \\ \dot{Y}_{EE} \\ \dot{\phi}_{EE} \end{pmatrix} \\ \dot{\theta}_{total} &= \dot{\theta}_{openloop} + K * \begin{cases} \begin{pmatrix} D_{1}_{desired} \\ D_{2}_{desired} \\ D_{3}_{desired} \\ \theta_{11}_{desired} \\ \theta_{12}_{desired} \\ \theta_{13}_{desired} \end{pmatrix} - \begin{pmatrix} D_{1} \\ D_{2} \\ D_{3} \\ \theta_{11} \\ \theta_{12} \\ \theta_{13} \end{pmatrix} \\ \dot{\theta}_{total} &= -inverse(B) * A * \begin{pmatrix} \dot{X}_{EE} \\ \dot{Y}_{EE} \\ \dot{\Phi}_{EE} \end{pmatrix} + K \\ & \left\{ \begin{pmatrix} D_{1}_{desired} \\ D_{2}_{desired} \\ \theta_{13}_{desired} \\ \theta_{13}_{desired} \\ \theta_{13}_{desired} \\ \theta_{13}_{desired} \end{pmatrix} - \begin{pmatrix} D_{1} \\ D_{2} \\ D_{3} \\ \theta_{11} \\ \theta_{12} \\ \theta_{13} \end{pmatrix} \right\} \end{split}$$





Please see drop box folder for code for closed loop control.



Please see drop box folder for code for closed loop control.

## 3) Closed Loop Control (Task Space):

$$\begin{split} \dot{\theta}_{closed} &= inverse(J) \\ & * \left\{ \begin{pmatrix} \dot{X}_{EE} \\ \dot{Y}_{EE} \\ \dot{\phi}_{EE} \end{pmatrix} + K * \left\{ \begin{pmatrix} X_{EE\,desired} \\ Y_{EE\,desired} \\ \phi_{EE\,desired} \end{pmatrix} - \begin{pmatrix} X_{EE} \\ Y_{EE} \\ \phi_{EE} \end{pmatrix} \right\} \right\} \end{split}$$

$$\begin{aligned} \dot{\theta}_{closed} &= -inverse(B) * A \\ &* \left\{ \begin{pmatrix} \dot{X}_{EE} \\ \dot{Y}_{EE} \\ \dot{\phi}_{EE} \end{pmatrix} + K * \left\{ \begin{pmatrix} X_{EE\,desired} \\ Y_{EE\,desired} \\ \phi_{EE\,desired} \end{pmatrix} - \begin{pmatrix} X_{EE} \\ Y_{EE} \\ \phi_{EE} \end{pmatrix} \right\} \right\} \end{aligned}$$





Please see drop box folder for code for closed loop control.



Timeline for  $(D_1, D_2, D_3, \theta_{11}, \theta_{12}, \theta_{13})$ 

Please see drop box folder for code for closed loop control.

#### Manipulability:

## The *Jacobian J and inverse(J*) are given by

J = -inverse(B) \* A

inverse(J) = -inverse(A) \* B

	/1	0	$-L_{21}\sin\theta_{31}$
where A =	1	0	$-L_{22}\sin\theta_{32}$
	1	0	$-L_{23}\sin\theta_{33}$
	0	1	$L_{21}\cos\theta_{31}$
	0	1	$L_{22}\cos\theta_{32}$
	$\setminus 0$	1	$L_{23} \cos \theta_{33}$ /

and B

	$\cos \theta_{11}$	0	0	$-L_{11}\sin\theta_{21}$	0	0
=	0	$\cos \theta_{12}$	0	0	$-L_{12}\sin\theta_{22}$	0
	0	0	$\cos \theta_{13}$	0	0	$-L_{13}\sin \theta$
	$\sin \theta_{11}$	0	0	$L_{11}\cos\theta_{21}$	0	0
	0	$\sin  heta_{12}$	0	0	$L_{12}\cos\theta_{22}$	0
	\ 0	0	$\sin  heta_{13}$	0	0	$L_{13}\cos\theta$

1) Yoshikawa Measure of Manipulability

 $YMOM = \sqrt[2]{\det(J * transpose(J))}$ 

For L = 5, R = 8



For L = 3, R = 6



Please see drop box folder for code for Yoshikawa measure of manipulability.



For L = 5, R = 8



For L = 3, R = 6



Please see drop box folder for code for Isotropy Index measure of manipulability.

#### <u>Appendix</u>

Forward Kinematics <u>http://www.youtube.com/watch?v=a7xhaL0nNgQ</u> Inverse Kinematics <u>http://www.youtube.com/watch?v=3Iui26pu7\_Q</u> Workspace <u>http://www.youtube.com/watch?v=X1XuG5JBSes</u> Circle/Ellipse tracing <u>http://www.youtube.com/watch?v=YgYIR9T2IIs</u> Open Loop Control <u>http://www.youtube.com/watch?v=nNBnEevXJQs</u> Task Space Closed Loop Control <u>http://www.youtube.com/watch?v=BIOhLbwaimY</u> Joint Space Closed Loop Control <u>http://www.youtube.com/watch?v=u6Es0GRB6dI</u> Isotropy Index Measure of Manipulability <u>http://www.youtube.com/watch?v=DrsB7A8xwBA</u>